# **IMPLEMENTATION OF UNBIASED FIR FILTERS WITH LOW-DEGREE POLYNOMIAL GAINS**

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# ABSTRACT

We discuss implementation of the unbiased finite impulse response (FIR) filters. The transfer function and general blockdiagram are presented for the *l*-degree polynomial FIR filter along with its fundamental properties in the z-transform domain. As a special results, we show a fundamental identity that is uniquely featured to such filters and can serve as an indicator of unbiasedness in filter design. For low-degree gains, the transfer function is represented in simple closed forms and compact block-diagrams. An example of applications is given for filtering of time errors in a crystal clock.

### 1. INTRODUCTION

Finite impulse response (FIR) estimators are commonly used whenever a linear phase response is required. Among known solutions, there is a special class of devices [1-3] intended for unbiased FIR filtering of oversampled signals. When such a filter is matched with the signal model, the group delay reaches a minimum. Otherwise, it grows with, however, lower rate than in the infinite impulse response (IIR) ones. The payment is a high order of FIR structures.

Simple implementation of FIR structures has become available after Heinonen and Neuvo designed the predictive FIR filters with polynomial gains [4]. These filters have been studied and used by many authors [5-9]. Later, Shmaliy showed in [10] that Heinonen-Neuvo's solution is unbiased and the theory of unbiased FIR estimators has been developed in [3, 10–13]. Most recently, in [14], it has been noticed that the unbiased FIR filter becomes virtually optimal when the number N of points in the average is large that makes it a useful engineering solution in optimal filtering.

Following [10], the unbiased FIR filtering estimate  $\hat{x}_{n|n}$  of an *l*-degree polynomial signal  $x_n$  can be found in the convolution form at a current discrete time point *n* via measurement  $y_n$  obtained from n - N + 1 to n as

$$\hat{x}_{n|n} = \sum_{i=0}^{N-1} h_{li} y_{n-i}, \qquad (1)$$

where the *l*-degree polynomial FIR filter gain  $h_{ln} \triangleq h_{ln}(N)$  is specified as

$$h_{ln} = \sum_{m=0}^{l} a_{ml} n^m \tag{2}$$

with the coefficient  $a_{ml} \triangleq a_{ml}(N)$ ,

$$a_{ml} = (-1)^m \frac{M_{(m+1)1}}{|\mathbf{D}|}, \qquad (3)$$

in which  $|\mathbf{D}| \triangleq |\mathbf{D}(N)|$  is the determinant and  $M_{(m+1)1} \triangleq$  $M_{(m+1)1}(N)$  is the minor of the  $(l+1) \times (l+1)$  quadratic matrix  $\mathbf{D} \triangleq \mathbf{D}(N)$ ,

$$\mathbf{D} = \begin{bmatrix} d_0 & d_1 & \dots & d_l \\ d_1 & d_2 & \dots & d_{l+1} \\ \vdots & \vdots & \ddots & \vdots \\ d_l & d_{l+1} & \dots & d_{2l} \end{bmatrix},$$
(4)

which generic component  $d_v = \sum_{i=0}^{N-1} i^v$ ,  $v \in [0, 2l]$ , is determined by the Bernoulli polynomials (see Appendix A in [10]). The gain (2), existing from zero to N - 1, has the following fundamental properties: the sum of its coefficients is unity,  $\sum_{n=0}^{N-1} h_{ln} = 1$ , and the moments are zeroth,

$$\sum_{n=0}^{N-1} h_{ln} n^u = 0, \quad 1 \leqslant u \leqslant l.$$
<sup>(5)</sup>

For low-degree polynomial signals, the unique ramp, quadratic, and cubic gains were originally found in [10–12] to be, respectively,

$$h_{1n} = \frac{2(2N-1)-6n}{N(N+1)}, \qquad (6)$$

$$h_{2n} = \frac{3(3N^2 - 3N + 2) - 18(2N - 1)n + 30n^2}{N(N+1)(N+2)}, \quad (7)$$

$$h_{3n} = \frac{8(2N^3 - 3N^2 + 7N - 3) - 20(6N^2 - 6N)}{N(N+1)(N+2)(N+3)}, (8)$$

and higher degree gains can be found similarly.

Below, we consider design and application of the unbiased FIR filters with low-degree gains (6)-(8), by finding closed-form transfer functions and compact block-diagrams.

# 2. TRANSFER FUNCTION OF THE UNBIASED FIR FILTER

The transfer function of the discrete-time *l*-degree unbiased FIR filter is specialized with the z-transform applied to the

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gain (2) as

$$H_l(z) = \sum_{n=0}^{N-1} h_{ln} z^{-n}$$
(9)

$$= \sum_{m=0}^{l} a_{lm} \sum_{n=0}^{N-1} n^{m} z^{-n}, \qquad (10)$$

where  $z = e^{j\omega T}$ ,  $\omega$  is the angular frequency, T is the sampling time, and  $a_{lm}$  is specified with (3). The following properties of  $H_l(z)$  can be listed in addition to the inherent ones of  $2\pi$ -periodicity, symmetry of  $|H_l(z)|$ , and asymmetry of  $\arg H_l(z)$ .

## **2.1 Transfer Function at** k = 0

By  $\omega = 0$ , we have z = 1 and, referring to (10) and (5), obtain

$$H_l(z) = 1 \tag{11}$$

for all *l*, meaning that the unbiased FIR filters is essentially an LP filter.

# **2.2** Filter Gain at n = 0

By the inverse *z*-transform, the value of  $h_{ln}$  at n = 0 becomes

$$h_{l0} = \frac{1}{2\pi j} \oint_{C_1} \frac{H_l(z)}{z} dz \qquad (12a)$$

$$= \frac{1}{2\pi} \int_{0}^{2\pi} H_l(e^{j\omega T}) d(\omega T).$$
(12b)

Because  $h_{l0}$  is positive,  $h_{l0} > 0$ , for all l and  $N \ge 2$  [10], the counterclockwise circular integration in (12a) always produces a positive imaginary value that gives us

$$\oint_{C_1} \frac{H_l(z)}{jz} dz = 2\pi h_{l0} > 0.$$
(13)

## **2.3** Transfer Function at $\omega T = \pi$

With  $\omega T = \pi$ , we have  $z^{-n} = e^{-j\pi n} = (-1)^n$  and provide

$$H_l(z=e^{j\pi}) = -\sum_{m=0}^l \frac{a_{lm}}{2} \left[ (-1)^N E_m(N) - E_m(0) \right], \quad (14)$$

where  $E_m(x)$  is the Euler polynomial. For most widely used the low-degree gains,  $0 \le l \le 3$ , the Euler polynomials are given with  $E_0(x) = 1$ ,  $E_1(x) = x - \frac{1}{2}$ ,  $E_2(x) = x^2 - x$ , and  $E_3(x) = x^3 - \frac{3}{2}x^2 + \frac{1}{4}$ .

# 2.4 Energy

If  $H_l(z)$  is the *z* transform of  $h_{ln}$ , then, by the Parceval theorem and (5), one has

$$\frac{1}{2\pi} \int_{0}^{2\pi} |H_{l}(e^{j\omega T})|^{2} d(\omega T) = \sum_{n=0}^{N-1} h_{ln}^{2}$$
$$= \sum_{j=0}^{l} a_{jl} \sum_{i=0}^{N-1} h_{li} i^{j}$$
$$= a_{0l} = h_{l0}, \qquad (15)$$



Figure 1: A generalized block-diagram of the *l*-degree unbiased FIR filter.

meaning that the gain energy in the transform domain is equal to the value of  $h_{ln}$  at n = 0. Comparing (15) and (13), one arrives at a noble identity

$$\int_{0}^{2\pi} H_l(e^{j\omega T}) d(\omega T) = \int_{0}^{2\pi} |H_l(e^{j\omega T})|^2 d(\omega T), \quad (16)$$

uniquely featured to the discrete-time unbiased FIR filters in the transform domain.

#### 2.5 Noise power gain

The noise power gain (NPG)  $g_l \triangleq g_l(N)$  is defined in [4] by the energy of  $h_{ln}$ , characterizing noise amount in the output of digital filters [15]. By Parceval's theorem and (16), the NPG can be evaluated in the following forms of

$$g_l = \frac{1}{2\pi} \int_{0}^{2\pi} |H_l(e^{j\omega T})|^2 d(\omega T)$$
 (17a)

$$= \frac{1}{2\pi} \int_{0}^{2\pi} H_l(e^{j\omega T}) d(\omega T)$$
(17b)

$$h_{l0} = a_{0l}$$
. (17c)

We notice that an analysis of  $g_l$  for  $0 \le l \le 3$  in the time domain is given in [10].

## 3. TRANSFER FUNCTIONS OF LOW-DEGREE FIR FILTERS

Although the inner sum in (10) has no closed form for arbitrary *m*, it can be shown that the general form of  $H_l(z)$  is

$$H_{l}(z) = \frac{\sum_{i=0}^{l} \beta_{i} z^{-i} + z^{-N} \sum_{i=0}^{l} \gamma_{i} z^{-i}}{1 + \sum_{i=1}^{l+1} \alpha_{i} z^{-i}}.$$
 (18)

By assigning

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$$H_{\beta l}(z) = \left(\sum_{i=0}^{l} \beta_{i} z^{-i}\right) / \left(1 + \sum_{i=1}^{l+1} \alpha_{i} z^{-i}\right), \quad (19)$$

$$H_{\gamma l}(z) = \left(\sum_{i=0}^{l} \gamma_i z^{-i}\right) / \left(1 + \sum_{i=1}^{l+1} \alpha_i z^{-i}\right), \quad (20)$$

we go to the generalized block-diagram of the *l*-degree unbiased FIR filter shown in Fig. 1. For low-degree gains,  $0 \le l \le 3$ , the coefficients in (18) are listed in Table 1, where  $a_{0l}$  can be defined by letting n = 0 in (6)–(8). That allows us to find the low-complexity block-diagrams for practical design of such filters with the ramp, quadratic, and cubic gains.

			l	
	0	1	2	3
$\beta_0$	$\frac{1}{N}$	$a_{01}$	<i>a</i> <sub>02</sub>	$a_{03}$
$\beta_1$	0	$-\frac{4}{N}$	$-\frac{18(N-1)}{N(N+1)}$	$-\frac{48(N^2-2N+2)}{N(N+1)(N+2)}$
$\beta_2$	0	0	$\frac{9}{N}$	$\frac{24(2N-3)}{N(N+1)}$
$\beta_3$	0	0	0	$-\frac{16}{N}$
<b>%</b>	$-\frac{1}{N}$	$\frac{2}{N}$	$-\frac{3}{N}$	$\frac{4}{N}$
$\gamma_1$	0	$-\frac{2(N-2)}{N(N+1)}$	$\frac{6(N-3)}{N(N+1)}$	$-\frac{12(N-4)}{N(N+1)}$
<b>Y</b> 2	0	0	$-\frac{3(N-2)(N-3)}{N(N+1)(N+2)}$	$\frac{12(N-3)(N-4)}{N(N+1)(N+2)}$
<b>Y</b> 3	0	0	0	$-\frac{4(N-2)(N-3)(N-4)}{N(N+1)(N+2)(N+3)}$
$\alpha_1$	-1	-2	-3	-4
$\alpha_2$	0	1	3	6
$\alpha_3$	0	0	-1	-4
$\alpha_{4}$	0	0	0	1

 Table 1: Transfer Function Coefficients of the Low-Degree

 Unbiased FIR Filters



Figure 2: Block-diagram of the ramp unbiased FIR filter.

# 3.1 Ramp Gain

The transfer function for the ramp FIR filter, l = 1, can be found in the following compact form, if to use Table 1 and provide the transformations in (18),

$$H_1(z) = \frac{2}{N} \frac{\frac{a_{01}N}{2} - 2z^{-1} + z^{-N} \left(1 - \frac{N-2}{N+1}z^{-1}\right)}{(1 - z^{-1})^2} \,. \tag{21}$$

A simple analysis shows that the region of convergence (ROC) in (21) is for all z and that the filter is both stable and causal. Fig. 2 sketches the relevant block-diagram, which structure is *N*-invariant, utilizing 6 multipliers, 4 adders, and 3 time-delays. The magnitude and phase responses of the ramp unbiased FIR filter, case l = 1, are illustrated in Fig. 3 and Fig. 4, respectively. Figure 3a assures us that the unbiasedness is achieved by shifting and elevating the side lobes of the uniform FIR filter, l = 0. The phase response of this filter is linear in average (Fig. 4a). However, its function oscillates, similarly to the predictive FIR filters [5–7], making the group delay also oscillating about a small constant value (Fig. 4b).



Figure 3: Magnitude response of the low-degree unbiased FIR filters: (a)  $|H_l(e^{j\omega T})|$  for N = 20 and (b) Bode plot of  $|H_l(e^{j\omega T})|^2$  in dB for N = 500.



Figure 4: Phase characteristics of the low-degree unbiased FIR filters for N = 20: (a) phase response  $\arg H_l(e^{j\omega T})$  and (b) group delay  $d[\arg H_l(e^{j\omega T})]/d(\omega T)$ .

$$H_2(z) = \frac{3}{N} \frac{\frac{a_{02}N}{3} - \frac{6(N-1)}{N+1}z^{-1} + 3z^{-2} - z^{-N} \left[1 - \frac{2(N-3)}{N+1}z^{-1} + \frac{(N-2)(N-3)}{(N+1)(N+2)}z^{-2}\right]}{(1-z^{-1})^3}.$$
(22)

$$H_{3}(z) = \frac{\frac{a_{03}N}{4} - \frac{12(N^{2} - 2N + 2)}{(N+1)(N+2)}z^{-1} + \frac{6(2N-3)}{N+1}z^{-2} - 4z^{-3} + z^{-N}\left(1 - b_{1}z^{-1} + b_{2}z^{-2} - b_{3}z^{-3}\right)}{N(1 - z^{-1})^{4}/4}.$$
(23)



Figure 5: Block-diagram of the unbiased FIR filter with a quadratic gain.



Figure 6: Block-diagram of the unbiased FIR filter with a cubic gain.

## 3.2 Quadratic Gain

After the routine transformations, the transfer function of the quadratic unbiased FIR filter becomes (22). The relevant block-diagram shown in Fig. 5 is performed with 9 multipliers, 5 adders, and 4 time-delays.

# 3.3 Cubic Gain

The unbiased FIR filter with a cubic gain, l = 3, can be represented with the transfer function (23), in which the coefficients are give by  $b_1 = \frac{3(N-4)}{N+1}$ ,  $b_2 = \frac{3(N-3)(N-4)}{(N+1)(N+2)}$ , and  $b_3 = \frac{(N-2)(N-3)(N-4)}{(N+1)(N+2)(N+3)}$ . The block-diagram corresponding to (23) is sketched in Fig. 6. It is easily indicated that this filter requires 12 multipliers, 5 adders, and 4 time-shifters. The magnitude and phase responses of the filter with a cubic gain are given in Fig. 3 and Fig. 4. Observing these figures, one can trace an evolution of the filter transfer function, by increasing the filter degree.



Figure 7: GPS-based unbiased FIR filtering of the crystal clock TIE: (a) near linear TIE behavior, (b) near quadratic TIE behavior, and (c) complex TIE behavior. Here "grey" plot represents the GPS-based measurement, "white" the reference trend, and "black" the estimate.

# 4. FILTERING OF CLOCK ERRORS

An experimental test of the unbiased FIR filters (Fig. 7) has been provided for the Global Positioning System (GPS)based measurement of the time interval error (TIE)  $x_n$  of a precision crystal clock employing the one pulse per second (1PPS) signals of the SynPaQ III GPS Timing Sensor and Stanford Frequency Counter SR620 in the presence of the sawtooth noise induced in the receiver. To obtain the reference trend, the TIE has been simultaneously measured for the Symmetricom Frequency Cesium Standard CsIII employing another SR620. The clock was identified to have two states and the ramp FIR filter (Fig. 2) was therefore used.

In the first experiment, we selected a part of the process in which the TIE of the OCXO-based clock change with almost a constant linear slope. Following [18], the time step was set to be 1 s and the optimum N was experimentally found to be N = 2060. As can be inferred from the observation of Fig. 7a, the ramp FIR filter applied to the sawtooth measurement allows for the root mean square error (RMSE) of about 1.6 ns that is substantially lower than in the sawtooth corrected measurement [19].

For the second experiment, we selected a region where the TIE changed almost quadratically. In contrast to the near linear TIE trend (Fig. 7a), the optimum N has appeared here to be about N = 920. Numerical calculation gives us the RMSE of about 8.0 ns. Note that larger filtering errors are caused in Fig. 7b by the GPS time temporary uncertainties neatly seen in the GPS-based measurement and that there are no uncertainties in the reference measurement.

We finally exploit a part of measurement with a complex behavior of the TIE. The GPS-based and reference measurements and the estimate are shown in Fig. 7c. For this case, the optimum N was ascertained to be N = 1150 and the RMSE calculated as 7.83 ns.

### 5. CONCLUDING REMARKS

In this paper, we discussed the discrete-time *l*-degree polynomial unbiased FIR filter, its transfer function, and a generalized block-diagram. Fundamental properties of the filter transfer function have also been studied. A special attention has been paid to the most widely used low-degree gains (ramp, quadratic, and cubic), in which case the transfer function has been represented in simple closed forms and in compact block-diagrams. The magnitude and phase responses of the low-degree filters have been analyzed and compared to those of the predictive unbiased FIR ones. As an example of applications, we discussed filtering of the crystal clock errors via the GPS-based measurement of the TIE. It has been demonstrated graphically that the filter output has no time delay with respect to the reference trend.

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